

# EE 565: Position, Navigation, and Timing

## INS Initialization

Aly El-Osery   Kevin Wedeward

Electrical Engineering Department, New Mexico Tech  
Socorro, New Mexico, USA

*In Collaboration with*  
Stephen Bruder

Electrical and Computer Engineering Department  
Embry-Riddle Aeronautical University  
Prescott, Arizona, USA

April 19, 2023

Position, velocity and attitude drift unless the INS is aided. There are some opportunistic situations that provide information to the INS to initialize itself. Two categories of alignment

- Coarse Alignment
- Fine Alignment

- 1 *Coarse Alignment*: Use knowledge of the gravity vector and earth rate provided by the three accelerometers, and the knowledge of the earth rate vector provided by the gyroscopes.
- 2 *Fine Alignment*: Needed in quasi-stationary situations. Uses the fact that any position, velocity changes are considered disturbances, and the knowledge of the gravity vector and earth rate to estimate the body's attitude.

Latitude needs to be known.

$$\vec{f}_{ib}^b = -C_n^b \begin{pmatrix} 0 \\ 0 \\ g \end{pmatrix} = \begin{pmatrix} \sin(\theta) \\ -\cos(\theta) \sin(\phi) \\ -\cos(\theta) \cos(\phi) \end{pmatrix} g$$

$$\vec{f}_{ib}^b = -C_n^b \begin{pmatrix} 0 \\ 0 \\ g \end{pmatrix} = \begin{pmatrix} \sin(\theta) \\ -\cos(\theta) \sin(\phi) \\ -\cos(\theta) \cos(\phi) \end{pmatrix} g$$

Only provides pitch and roll angles  
 $g$  (+ve)

$$\left( \tilde{\vec{f}}_{ib}^b, \tilde{\vec{\omega}}_{ib}^b, \tilde{\vec{f}}_{ib}^b \times \tilde{\vec{\omega}}_{ib}^b \right) =$$

$$\left( \tilde{\vec{f}}_{ib}^b, \tilde{\vec{\omega}}_{ib}^b, \tilde{\vec{f}}_{ib}^b \times \tilde{\vec{\omega}}_{ib}^b \right) = \hat{C}_n^b \left( \vec{f}_{ib}^n, \vec{\omega}_{ib}^n, \vec{f}_{ib}^n \times \vec{\omega}_{ib}^n \right)$$

$$\left( \vec{f}_{ib}^b, \vec{\omega}_{ib}^b, \vec{f}_{ib}^b \times \vec{\omega}_{ib}^b \right) = \hat{C}_n^b \left( \vec{f}_{ib}^n, \vec{\omega}_{ib}^n, \vec{f}_{ib}^n \times \vec{\omega}_{ib}^n \right)$$

$$\hat{C}_n^b = \begin{pmatrix} C_{11} & C_{12} & C_{13} \\ C_{21} & C_{22} & C_{23} \\ C_{31} & C_{32} & C_{33} \end{pmatrix}$$



$$\left( \tilde{\vec{f}}_{ib}^b, \tilde{\vec{\omega}}_{ib}^b, \tilde{\vec{f}}_{ib}^b \times \tilde{\vec{\omega}}_{ib}^b \right) = \hat{C}_n^b \left( \vec{f}_{ib}^n, \vec{\omega}_{ib}^n, \vec{f}_{ib}^n \times \vec{\omega}_{ib}^n \right)$$

$$\hat{C}_n^b = \begin{pmatrix} C_{11} & C_{12} & C_{13} \\ C_{21} & C_{22} & C_{23} \\ C_{31} & C_{32} & C_{33} \end{pmatrix}$$

where

$$C_{11} = \frac{\tilde{\omega}_x^b}{\omega_{ie} \cos(L_b)} - \frac{\tilde{f}_x^b \tan(L_b)}{g}$$

$$C_{12} = \frac{\tilde{f}_z^b \tilde{\omega}_y^b - \tilde{f}_y^b \tilde{\omega}_z^b}{g \omega_{ie} \cos(L_b)}$$

$$C_{13} = \frac{-\tilde{f}_x^b}{g}$$

$$C_{21} = \frac{\tilde{\omega}_y^b}{\omega_{ie} \cos(L_b)} - \frac{\tilde{f}_y^b \tan(L_b)}{g}$$

$$C_{22} = \frac{-\tilde{f}_z^b \tilde{\omega}_x^b + \tilde{f}_x^b \tilde{\omega}_z^b}{g \omega_{ie} \cos(L_b)}$$

$$C_{23} = \frac{-\tilde{f}_y^b}{g}$$

$$C_{31} = \frac{\tilde{\omega}_z^b}{\omega_{ie} \cos(L_b)} - \frac{\tilde{f}_z^b \tan(L_b)}{g}$$

$$C_{32} = \frac{\tilde{f}_y^b \tilde{\omega}_x^b - \tilde{f}_x^b \tilde{\omega}_y^b}{g \omega_{ie} \cos(L_b)}$$

$$C_{33} = \frac{-\tilde{f}_z^b}{g}$$

Must ensure that the DCM is properly orthogonalized.

- Use full INS mechanization
- Use equivalent to GPS aided error mechanization
- Setup up measurements

- Use full INS mechanization
- Use equivalent to GPS aided error mechanization
- Setup up measurements
  - ① Specific force measurement

$$\delta \vec{f}_{ib}^b = \vec{f}_{ib}^b - \hat{\vec{f}}_{ib}^b$$

- Use full INS mechanization
- Use equivalent to GPS aided error mechanization
- Setup up measurements
  - 1 Specific force measurement

$$\delta \vec{f}_{ib}^b = \vec{f}_{ib}^b - \hat{\vec{f}}_{ib}^b$$

- 2 Angular rate measurement

$$\delta \vec{\omega}_{ib}^b = \vec{\omega}_{ib}^b - \hat{\vec{\omega}}_{ib}^b$$

- Use full INS mechanization
- Use equivalent to GPS aided error mechanization
- Setup up measurements

- 1 Specific force measurement

$$\delta \vec{f}_{ib}^b = \vec{f}_{ib}^b - \hat{\vec{f}}_{ib}^b$$

- 2 Angular rate measurement

$$\delta \vec{\omega}_{ib}^b = \vec{\omega}_{ib}^b - \hat{\vec{\omega}}_{ib}^b$$

- 3 Position measurement: deviation from initial position

- Use full INS mechanization
- Use equivalent to GPS aided error mechanization
- Setup up measurements

- 1 Specific force measurement

$$\delta \vec{f}_{ib}^b = \vec{f}_{ib}^b - \hat{\vec{f}}_{ib}^b$$

- 2 Angular rate measurement

$$\delta \vec{\omega}_{ib}^b = \vec{\omega}_{ib}^b - \hat{\vec{\omega}}_{ib}^b$$

- 3 Position measurement: deviation from initial position
- 4 Velocity measurement: deviation from zero

$$\begin{aligned}\delta \vec{f}_{ib}^n &= \vec{f}_{ib}^n - \hat{\vec{f}}_{ib}^n \\ &= \vec{f}_{ib}^n - (I - [\delta \vec{\psi}_{nb}^n \times]) C_b^n (\vec{f}_{ib}^b - \delta \vec{f}_{ib}^b) + f_d \\ &= [\delta \vec{\psi}_{nb}^n \times] C_b^n \vec{f}_{ib}^b + \hat{C}_b^n \delta \vec{f}_{ib}^b + f_d\end{aligned}$$

$$\begin{aligned}
 \delta \vec{f}_{ib}^n &= \vec{f}_{ib}^n - \hat{\vec{f}}_{ib}^n \\
 &= \vec{f}_{ib}^n - (I - [\delta \vec{\psi}_{nb}^n \times]) C_b^n (\vec{f}_{ib}^b - \delta \vec{f}_{ib}^b) + f_d \\
 \hat{C}_b^n &= [\delta \vec{\psi}_{nb}^n \times] C_b^n \vec{f}_{ib}^b + \hat{C}_b^n \delta \vec{f}_{ib}^b + f_d \\
 &= \begin{pmatrix} 0 & -\delta\psi_D & \delta\psi_E \\ \delta\psi_D & 0 & -\delta\psi_N \\ -\delta\psi_E & \delta\psi_N & 0 \end{pmatrix} \begin{pmatrix} 0 \\ 0 \\ -g \end{pmatrix} + \hat{C}_b^n \delta \vec{f}_{ib}^b + f_d
 \end{aligned}$$



$$\begin{aligned}
 \delta \vec{f}_{ib}^n &= \vec{f}_{ib}^n - \hat{\vec{f}}_{ib}^n \\
 &= \vec{f}_{ib}^n - (I - [\delta \vec{\psi}_{nb}^n \times]) C_b^n (\vec{f}_{ib}^b - \delta \vec{f}_{ib}^b) + f_d \\
 &= [\delta \vec{\psi}_{nb}^n \times] C_b^n \vec{f}_{ib}^b + \hat{C}_b^n \delta \vec{f}_{ib}^b + f_d \\
 &= \begin{pmatrix} 0 & -\delta \psi_D & \delta \psi_E \\ \delta \psi_D & 0 & -\delta \psi_N \\ -\delta \psi_E & \delta \psi_N & 0 \end{pmatrix} \begin{pmatrix} 0 \\ 0 \\ -g \end{pmatrix} + \hat{C}_b^n \delta \vec{f}_{ib}^b + f_d \\
 &= \begin{pmatrix} 0 & -g & 0 \\ g & 0 & 0 \\ 0 & 0 & 0 \end{pmatrix} \begin{pmatrix} \delta \psi_N \\ \delta \psi_E \\ \delta \psi_D \end{pmatrix} + \hat{C}_b^n \delta \vec{f}_{ib}^b + f_d \\
 &= G \delta \vec{\psi}_{nb}^n + \hat{C}_b^n \delta \vec{f}_{ib}^b + f_d^b
 \end{aligned}$$

$$\begin{aligned}
 \delta \vec{f}_{ib}^n &= \vec{f}_{ib}^n - \hat{\vec{f}}_{ib}^n \\
 &= \vec{f}_{ib}^n - (I - [\delta \vec{\psi}_{nb}^n \times]) C_b^n (\vec{f}_{ib}^b - \delta \vec{f}_{ib}^b) + f_d \\
 &= [\delta \vec{\psi}_{nb}^n \times] C_b^n \vec{f}_{ib}^b + \hat{C}_b^n \delta \vec{f}_{ib}^b + f_d \\
 &= \begin{pmatrix} 0 & -\delta \psi_D & \delta \psi_E \\ \delta \psi_D & 0 & -\delta \psi_N \\ -\delta \psi_E & \delta \psi_N & 0 \end{pmatrix} \begin{pmatrix} 0 \\ 0 \\ -g \end{pmatrix} + \hat{C}_b^n \delta \vec{f}_{ib}^b + f_d \\
 &= \begin{pmatrix} 0 & -g & 0 \\ g & 0 & 0 \\ 0 & 0 & 0 \end{pmatrix} \begin{pmatrix} \delta \psi_N \\ \delta \psi_E \\ \delta \psi_D \end{pmatrix} + \hat{C}_b^n \delta \vec{f}_{ib}^b + f_d \\
 &= G \delta \vec{\psi}_{nb}^n + \hat{C}_b^n \delta \vec{f}_{ib}^b + f_d^b
 \end{aligned}$$

Recoordinatize in the body frame

$$\delta \vec{f}_{nb}^b = \hat{C}_n^b G \delta \vec{\psi}_{nb}^n + \delta \vec{f}_{ib}^b + \vec{f}_d^b$$

$\delta \vec{f}_{ib}^b$  captures bias-drift (sinking) + Markov, ..., and  $f_d$  represents variations in the nav frame

$$\delta\vec{\omega}_{in}^n = \vec{\omega}_{in}^n - \hat{\omega}_{in}^n$$

$$\begin{aligned}\delta\vec{\omega}_{in}^n &= \vec{\omega}_{in}^n - \hat{\vec{\omega}}_{in}^n \\ &= (I + [\delta\vec{\psi}_{nb}^n \times]) \hat{C}_b^n (\vec{\omega}_{ib}^b + \vec{\omega}_{bn}^b) - \hat{C}_b^n (\vec{\omega}_{ib}^b - \delta\vec{\omega}_{ib}^b)\end{aligned}$$

$$\begin{aligned}\delta\vec{\omega}_{in}^n &= \vec{\omega}_{in}^n - \hat{\omega}_{in}^n \\ &= (I + [\delta\vec{\psi}_{nb}^n \times]) \hat{C}_b^n (\vec{\omega}_{ib}^b + \vec{\omega}_{bn}^b) - \hat{C}_b^n (\vec{\omega}_{ib}^b - \delta\vec{\omega}_{ib}^b)\end{aligned}$$

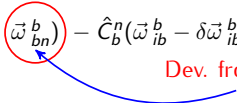
$C_b^n$  →

$$\begin{aligned}
 \delta \vec{\omega}_{in}^n &= \vec{\omega}_{in}^n - \hat{\vec{\omega}}_{in}^n \\
 &= (I + [\delta \vec{\psi}_{nb}^n \times]) \hat{C}_b^n (\vec{\omega}_{ib}^b + \vec{\omega}_{bn}^b) - \hat{C}_b^n (\vec{\omega}_{ib}^b - \delta \vec{\omega}_{ib}^b)
 \end{aligned}$$

$\hat{\vec{\omega}}_{ib}^n = \hat{\vec{\omega}}_{ie}^n$

$$\begin{aligned}\delta\vec{\omega}_{in}^n &= \vec{\omega}_{in}^n - \hat{\vec{\omega}}_{in}^n \\ &= (I + [\delta\vec{\psi}_{nb}^n \times]) \hat{C}_b^n (\vec{\omega}_{ib}^b + \vec{\omega}_{bn}^b) - \hat{C}_b^n (\vec{\omega}_{ib}^b - \delta\vec{\omega}_{ib}^b)\end{aligned}$$

Dev. from stationarity



$$\begin{aligned}
 \delta \vec{\omega}_{in}^n &= \vec{\omega}_{in}^n - \hat{\vec{\omega}}_{in}^n \\
 &= (I + [\delta \vec{\psi}_{nb}^n \times]) \hat{C}_b^n (\vec{\omega}_{ib}^b + \vec{\omega}_{bn}^b) - \hat{C}_b^n (\vec{\omega}_{ib}^b - \delta \vec{\omega}_{ib}^b) \\
 &= \begin{pmatrix} 0 & \Omega_D & 0 \\ -\Omega_D & 0 & \Omega_N \\ 0 & -\Omega_N & 0 \end{pmatrix} \begin{pmatrix} \delta \psi_N \\ \delta \psi_E \\ \delta \psi_D \end{pmatrix} + \hat{C}_b^n \delta \vec{\omega}_{ib}^b - \vec{\omega}_d^n \\
 &= W \delta \vec{\psi}_{nb}^n + \hat{C}_b^n \delta \vec{\omega}_{ib}^b - \vec{\omega}_d^n
 \end{aligned}$$



$$\begin{aligned}
 \delta \vec{\omega}_{in}^n &= \vec{\omega}_{in}^n - \hat{\vec{\omega}}_{in}^n \\
 &= (I + [\delta \vec{\psi}_{nb}^n \times]) \hat{C}_b^n (\vec{\omega}_{ib}^b + \vec{\omega}_{bn}^b) - \hat{C}_b^n (\vec{\omega}_{ib}^b - \delta \vec{\omega}_{ib}^b) \\
 &= \begin{pmatrix} 0 & \Omega_D & 0 \\ -\Omega_D & 0 & \Omega_N \\ 0 & -\Omega_N & 0 \end{pmatrix} \begin{pmatrix} \delta \psi_N \\ \delta \psi_E \\ \delta \psi_D \end{pmatrix} + \hat{C}_b^n \delta \vec{\omega}_{ib}^b - \vec{\omega}_d^n \\
 &= W \delta \vec{\psi}_{nb}^n + \hat{C}_b^n \delta \vec{\omega}_{ib}^b - \vec{\omega}_d^n
 \end{aligned}$$

Recoordinatize in the body frame

$$\delta \vec{\omega}_{in}^b = \hat{C}_n^b W \delta \vec{\psi}_{nb}^n + \delta \vec{\omega}_{ib}^b - \vec{\omega}_d^b$$

$\delta \vec{\omega}_{ib}^b$  captures bias-drift (sinking) + Markov, ...,  $\vec{\omega}_d$  represents variations from stationarity.

$$\dot{\vec{x}}(t) = F(t)\vec{x}(t) + \vec{w}(t)$$

$$\vec{y}(t) = H(t)\vec{x}(t) + \vec{v}(t)$$

$$\vec{x} = \left( \delta\vec{\psi}_{nb}^n \quad \delta\vec{v}_{nb}^n \quad \delta\vec{r}_{nb}^n \quad \vec{b}_a \quad \vec{b}_g \right)^T$$

$$H = \begin{pmatrix} 0_{3 \times 3} & 0_{3 \times 3} & I_{3 \times 3} & 0_{3 \times 3} & 0_{3 \times 3} \\ 0_{3 \times 3} & I_{3 \times 3} & 0_{3 \times 3} & 0_{3 \times 3} & 0_{3 \times 3} \\ \hat{C}_n^b G & 0_{3 \times 3} & 0_{3 \times 3} & I_{3 \times 3} & 0_{3 \times 3} \\ \hat{C}_n^b W & 0_{3 \times 3} & 0_{3 \times 3} & 0_{3 \times 3} & I_{3 \times 3} \end{pmatrix}$$

where the measurements are: position error, velocity error, specific force error, and angular velocity errors, respectively.

There is no mechanism in the above formulation to estimate  $\vec{\omega}_d^n$ . If it can be modelled as white noise then the filter will be able to handle it. On the other hand, if it is correlated type of disturbance, additional measures must be taken to account for it.