

# EE 570: Location and Navigation

## Error Mechanization (ECEF)

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Attitude	Velocity	Gravity	Position	Summary
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$$\dot{C}_b^e = C_b^e \Omega_{eb}^b = C_b^e (\Omega_{ib}^b - \Omega_{ie}^b) = \frac{d}{dt} [(\mathcal{I} + [\delta \vec{\psi}_{eb}^e \times]) \hat{C}_b^e] :$$

$$\dot{C}_b^e = C_b^e \Omega_{eb}^b = C_b^e (\Omega_{ib}^b - \Omega_{ie}^b) = \frac{d}{dt} [(\mathcal{I} + [\delta \vec{\psi}_{eb}^e \times]) \hat{C}_b^e] =$$

$$(\mathcal{I} + [\delta \vec{\psi}_{eb}^e \times]) \hat{C}_b^e \Omega_{eb}^b = [\dot{\delta \vec{\psi}}_{eb}^e \times] \hat{C}_b^e + (\mathcal{I} + [\delta \vec{\psi}_{eb}^e \times]) \dot{\hat{C}}_b^e =$$

$$\dot{C}_b^e = C_b^e \Omega_{eb}^b = C_b^e (\Omega_{ib}^b - \Omega_{ie}^b) = \frac{d}{dt} [(\mathcal{I} + [\delta \vec{\psi}_{eb}^e \times]) \hat{C}_b^e] =$$

$$(\mathcal{I} + [\delta \vec{\psi}_{eb}^e \times]) \hat{C}_b^e \Omega_{eb}^b = [\dot{\delta \vec{\psi}}_{eb}^e \times] \hat{C}_b^e + (\mathcal{I} + [\delta \vec{\psi}_{eb}^e \times]) \dot{\hat{C}}_b^e = \\ \approx (\mathcal{I} + [\delta \vec{\psi}_{eb}^e \times]) \hat{C}_b^e (\hat{\Omega}_{eb}^b + \delta \Omega_{ib}^b - \delta \Omega_{ie}^b)$$

$$\dot{C}_b^e = C_b^e \Omega_{eb}^b = C_b^e (\Omega_{ib}^b - \Omega_{ie}^b) = \frac{d}{dt} [(\mathcal{I} + [\delta \vec{\psi}_{eb}^e \times]) \hat{C}_b^e] =$$

$$\begin{aligned}
 & (\mathcal{I} + [\delta \vec{\psi}_{eb}^e \times]) \hat{C}_b^e \Omega_{eb}^b = [\dot{\delta \vec{\psi}}_{eb}^e \times] \hat{C}_b^e + (\mathcal{I} + [\delta \vec{\psi}_{eb}^e \times]) \dot{\hat{C}}_b^e = \\
 & \approx (\mathcal{I} + [\delta \vec{\psi}_{eb}^e \times]) \hat{C}_b^e (\hat{\Omega}_{eb}^b + \delta \Omega_{ib}^b - \delta \Omega_{ie}^b) \\
 & \approx (\mathcal{I} + [\delta \vec{\psi}_{eb}^e \times]) \hat{C}_b^e \hat{\Omega}_{eb}^b + \hat{C}_b^e (\delta \Omega_{ib}^b - \delta \Omega_{ie}^b) \quad \therefore [\delta \vec{\psi}_{eb}^e \times] \delta \Omega_{eb}^b \approx 0
 \end{aligned}$$

$$\dot{C}_b^e = C_b^e \Omega_{eb}^b = C_b^e (\Omega_{ib}^b - \Omega_{ie}^b) = \frac{d}{dt} [(\mathcal{I} + [\delta \vec{\psi}_{eb}^e \times]) \hat{C}_b^e] =$$

$$\begin{aligned}
 & (\mathcal{I} + [\delta \vec{\psi}_{eb}^e \times]) \hat{C}_b^e \Omega_{eb}^b = [\dot{\delta \vec{\psi}}_{eb}^e \times] \hat{C}_b^e + (\mathcal{I} + [\delta \vec{\psi}_{eb}^e \times]) \dot{\hat{C}}_b^e = \\
 & \approx (\mathcal{I} + [\delta \vec{\psi}_{eb}^e \times]) \hat{C}_b^e (\Omega_{eb}^b + \delta \Omega_{ib}^b - \delta \Omega_{ie}^b) \\
 & \approx (\mathcal{I} + [\delta \vec{\psi}_{eb}^e \times]) \hat{C}_b^e \hat{\Omega}_{eb}^b + \hat{C}_b^e (\delta \Omega_{ib}^b - \delta \Omega_{ie}^b)
 \end{aligned}$$

= 

$$\dot{C}_b^e = C_b^e \Omega_{eb}^b = C_b^e (\Omega_{ib}^b - \Omega_{ie}^b) = \frac{d}{dt} [(\mathcal{I} + [\delta \vec{\psi}_{eb}^e \times]) \hat{C}_b^e] =$$

$$\begin{aligned}
 & (\mathcal{I} + [\delta \vec{\psi}_{eb}^e \times]) \hat{C}_b^e \Omega_{eb}^b = [\dot{\delta \vec{\psi}}_{eb}^e \times] \hat{C}_b^e + (\mathcal{I} + [\delta \vec{\psi}_{eb}^e \times]) \dot{\hat{C}}_b^e = \\
 & \approx (\mathcal{I} + [\delta \vec{\psi}_{eb}^e \times]) \hat{C}_b^e (\hat{\Omega}_{eb}^b + \delta \Omega_{ib}^b - \delta \Omega_{ie}^b) \\
 & \approx (\mathcal{I} + [\delta \vec{\psi}_{eb}^e \times]) \hat{C}_b^e \hat{\Omega}_{eb}^b + \hat{C}_b^e (\delta \Omega_{ib}^b - \delta \Omega_{ie}^b)
 \end{aligned}$$

$$[\dot{\delta \vec{\psi}}_{eb}^e \times] = \hat{C}_b^e (\delta \Omega_{ib}^b - \delta \Omega_{ie}^b) \hat{C}_b^e = [\hat{C}_b^e (\delta \vec{\omega}_{ib}^b - \delta \vec{\omega}_{ie}^b) \times] \quad (1)$$

$$\dot{C}_b^e = C_b^e \Omega_{eb}^b = C_b^e (\Omega_{ib}^b - \Omega_{ie}^b) = \frac{d}{dt} [(\mathcal{I} + [\delta \vec{\psi}_{eb}^e \times]) \hat{C}_b^e] =$$

$$\begin{aligned}
 & (\mathcal{I} + [\delta \vec{\psi}_{eb}^e \times]) \hat{C}_b^e \Omega_{eb}^b = [\dot{\delta \vec{\psi}}_{eb}^e \times] \hat{C}_b^e + (\mathcal{I} + [\delta \vec{\psi}_{eb}^e \times]) \dot{\hat{C}}_b^e = \\
 & \approx (\mathcal{I} + [\delta \vec{\psi}_{eb}^e \times]) \hat{C}_b^e (\hat{\Omega}_{eb}^b + \delta \Omega_{ib}^b - \delta \Omega_{ie}^b) \\
 & \approx (\mathcal{I} + [\delta \vec{\psi}_{eb}^e \times]) \hat{C}_b^e \hat{\Omega}_{eb}^b + \hat{C}_b^e (\delta \Omega_{ib}^b - \delta \Omega_{ie}^b)
 \end{aligned}$$

$$[\dot{\delta \vec{\psi}}_{eb}^e \times] = \hat{C}_b^e (\delta \Omega_{ib}^b - \delta \Omega_{ie}^b) \hat{C}_b^e = [\hat{C}_b^e (\delta \vec{\omega}_{ib}^b - \delta \vec{\omega}_{ie}^b) \times] \quad (1)$$

$$\dot{\delta \vec{\psi}}_{eb}^e = \hat{C}_b^e (\delta \vec{\omega}_{ib}^b - \delta \vec{\omega}_{ie}^b) \quad (2)$$

$$\begin{aligned}\dot{\delta\vec{\psi}}_{eb}^e &= \hat{C}_b^e(\delta\omega_{ib}^b - \delta\vec{\omega}_{ie}^b) \\ &= \hat{C}_b^e\delta\omega_{ib}^b - \hat{C}_b^e(\vec{\omega}_{ie}^b - \hat{\vec{\omega}}_{ie}^b) \\ &= \hat{C}_b^e\delta\omega_{ib}^b - (\hat{C}_b^e C_e^b - \mathcal{I})\vec{\omega}_{ie}^e \\ &= \hat{C}_b^e\delta\omega_{ib}^b + \delta\vec{\psi}_{eb}^e \times \vec{\omega}_{ie}^e\end{aligned}$$

$$\begin{aligned}
 \dot{\delta\vec{\psi}}_{eb}^e &= \hat{C}_b^e (\delta\omega_{ib}^b - \delta\vec{\omega}_{ie}^b) \\
 &= \hat{C}_b^e \delta\omega_{ib}^b - \hat{C}_b^e (\vec{\omega}_{ie}^b - \hat{\vec{\omega}}_{ie}^b) \\
 &= \hat{C}_b^e \delta\omega_{ib}^b - (\hat{C}_b^e C_e^b - \mathcal{I}) \vec{\omega}_{ie}^e \\
 &= \hat{C}_b^e \delta\omega_{ib}^b + \delta\vec{\psi}_{eb}^e \times \vec{\omega}_{ie}^e
 \end{aligned}$$

$$\dot{\delta\vec{\psi}}_{eb}^e = \hat{C}_b^e \delta\omega_{ib}^b - \vec{\Omega}_{ie}^e \delta\vec{\psi}_{eb}^e \quad (3)$$

$$\dot{\vec{v}}_{eb}^e = C_b^e \vec{f}_{ib}^b + \vec{g}_b^e - 2\Omega_{ie}^e \vec{v}_{eb}^e \quad (4)$$

$$\begin{aligned}\dot{\hat{v}}_{eb}^e &= \hat{C}_b^e \hat{\vec{f}}_{ib}^b + \hat{\vec{g}}_b^e - 2\Omega_{ie}^e \hat{v}_{eb}^e \\ &= (\mathcal{I} - [\delta\vec{\psi}_{eb}^e \times]) C_b^e (\vec{f}_{ib}^b - \delta\vec{f}_{ib}^b) + \hat{\vec{g}}_b^e - 2\Omega_{ie}^e \hat{v}_{eb}^e\end{aligned} \quad (5)$$

$$\dot{\vec{v}}_{eb}^e = C_b^e \vec{f}_{ib}^b + \vec{g}_b^e - 2\Omega_{ie}^e \vec{v}_{eb}^e \quad (4)$$

$$\begin{aligned} \dot{\hat{v}}_{eb}^e &= \hat{C}_b^e \hat{\vec{f}}_{ib}^b + \hat{\vec{g}}_b^e - 2\Omega_{ie}^e \hat{v}_{eb}^e \\ &= (\mathcal{I} - [\delta\vec{\psi}_{eb}^e \times]) C_b^e (\vec{f}_{ib}^b - \delta\vec{f}_{ib}^b) + \hat{\vec{g}}_b^e - 2\Omega_{ie}^e \hat{v}_{eb}^e \end{aligned} \quad (5)$$

$$\begin{aligned} \dot{\delta v}_{eb}^e &= \dot{\vec{v}}_{eb}^e - \dot{\hat{v}}_{eb}^e = [\delta\vec{\psi}_{eb}^e \times] C_b^e \vec{f}_{ib}^b + \hat{C}_b^e \delta\vec{f}_{ib}^b + \delta\vec{g}_b^e - 2\Omega_{ie}^e \delta\vec{v}_{eb}^e \\ &= [\delta\vec{\psi}_{eb}^e \times] \hat{C}_b^e \hat{\vec{f}}_{ib}^b + \hat{C}_b^e \delta\vec{f}_{ib}^b + \delta\vec{g}_b^e - 2\Omega_{ie}^e \delta\vec{v}_{eb}^e \end{aligned}$$

$$\dot{\vec{v}}_{eb}^e = C_b^e \vec{f}_{ib}^b + \vec{g}_b^e - 2\Omega_{ie}^e \vec{v}_{eb}^e \quad (4)$$

$$\begin{aligned} \dot{\hat{v}}_{eb}^e &= \hat{C}_b^e \hat{\vec{f}}_{ib}^b + \hat{\vec{g}}_b^e - 2\Omega_{ie}^e \hat{\vec{v}}_{eb}^e \\ &= (\mathcal{I} - [\delta\vec{\psi}_{eb}^e \times]) C_b^e (\vec{f}_{ib}^b - \delta\vec{f}_{ib}^b) + \hat{\vec{g}}_b^e - 2\Omega_{ie}^e \hat{\vec{v}}_{eb}^e \end{aligned} \quad (5)$$

$$\begin{aligned} \dot{\vec{v}}_{eb}^e &= \dot{\vec{v}}_{eb}^e - \dot{\hat{v}}_{eb}^e = [\delta\vec{\psi}_{eb}^e \times] C_b^e \vec{f}_{ib}^b + \hat{C}_b^e \delta\vec{f}_{ib}^b + \delta\vec{g}_b^e - 2\Omega_{ie}^e \delta\vec{v}_{eb}^e \\ &= [\delta\vec{\psi}_{eb}^e \times] \hat{C}_b^e \hat{\vec{f}}_{ib}^b + \hat{C}_b^e \delta\vec{f}_{ib}^b + \delta\vec{g}_b^e - 2\Omega_{ie}^e \delta\vec{v}_{eb}^e \end{aligned}$$

$$\dot{\vec{v}}_{eb}^e = -[\hat{C}_b^e \hat{\vec{f}}_{ib}^b \times] \delta\vec{\psi}_{eb}^e + \hat{C}_b^e \delta\vec{f}_{ib}^b + \delta\vec{g}_b^e - 2\Omega_{ie}^e \hat{\vec{v}}_{eb}^e \quad (6)$$

$$\delta \vec{g}_b^e \approx \frac{2g_0(\hat{L}_b)}{r_{eS}^e(\hat{L}_b)} \frac{\hat{r}_{eb}^e}{|\hat{r}_{eb}^e|^2} (\hat{r}_{eb}^e)^T \delta \vec{r}_{eb}^e \quad (7)$$

$$\dot{\vec{r}}_{eb}^e = \vec{v}_{eb}^e \quad (8)$$

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$$\dot{\vec{r}}_{eb}^e = \vec{v}_{eb}^e \quad (9)$$

# Summary - in terms of $\delta\vec{f}_{ib}^b$ , $\delta\vec{\omega}_{ib}^b$

$$\begin{pmatrix} \dot{\vec{\psi}}_{eb}^e \\ \dot{\vec{V}}_{eb}^e \\ \dot{\vec{r}}_{eb}^e \end{pmatrix} = \begin{bmatrix} -\Omega_{ie}^e & 0_{3 \times 3} & 0_{3 \times 3} \\ -[\hat{C}_b^e \hat{\vec{f}}_{ib}^b \times] & -2\Omega_{ie}^e & \frac{2g_0(\hat{L}_b)}{r_{es}^e(\hat{L}_b)} \frac{\hat{\vec{r}}_{eb}^e}{|\hat{\vec{r}}_{eb}^e|^2} (\hat{\vec{r}}_{eb}^e)^T \\ 0_{3 \times 3} & \mathcal{I}_{3 \times 3} & 0_{3 \times 3} \end{bmatrix} \begin{pmatrix} \delta\vec{\psi}_{eb}^e \\ \delta\vec{V}_{eb}^e \\ \delta\vec{r}_{eb}^e \end{pmatrix} + \\
 \begin{bmatrix} 0 & \hat{C}_b^e \\ \hat{C}_b^e & 0 \\ 0 & 0 \end{bmatrix} \begin{pmatrix} \delta\vec{f}_{ib}^b \\ \delta\vec{\omega}_{ib}^b \end{pmatrix} \quad (10)$$

- Truth value

$$\vec{x}$$

- Measured value

$$\tilde{\vec{x}}$$

- Estimated or computed value

$$\hat{\vec{x}}$$

- Error

$$\delta \vec{x} = \vec{x} - \hat{\vec{x}}$$

- Truth value 
  - Measured value  $\tilde{\vec{x}}$
  - Estimated or computed value  $\hat{\vec{x}}$
  - Error 
$$\delta \vec{x} = \vec{x} - \hat{\vec{x}}$$
- Nothing above

- Truth value

 $\vec{x}$ 

- Measured value



→ Use “tilde”

 $\hat{x}$ 

- Estimated or computed value

- Error

$$\delta \vec{x} = \vec{x} - \hat{x}$$

- Truth value

$$\vec{x}$$

- Measured value

$$\tilde{\vec{x}}$$

- Estimated or computed value



“Use hat”

- Error

$$\delta \vec{x} = \vec{x} - \hat{\vec{x}}$$

- Truth value

$$\vec{x}$$

- Measured value

$$\tilde{\vec{x}}$$

- Estimated or computed value

$$\hat{\vec{x}}$$

- Error

$$\delta \vec{x} = \vec{x} - \hat{\vec{x}}$$

Given a non-linear system  $\dot{\vec{x}} = f(\vec{x}, t)$

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Let's assume we have an estimate of  $\vec{x}$ , i.e.,  $\hat{\vec{x}}$  such that  $\vec{x} = \hat{\vec{x}} + \delta\vec{x}$

$$\dot{\vec{x}} = \dot{\hat{\vec{x}}} + \dot{\delta\vec{x}} = f(\hat{\vec{x}} + \delta\vec{x}, t) \quad (11)$$

Given a non-linear system  $\dot{\vec{x}} = f(\vec{x}, t)$

Let's assume we have an estimate of  $\vec{x}$ , i.e.,  $\hat{\vec{x}}$  such that  $\vec{x} = \hat{\vec{x}} + \delta\vec{x}$

$$\dot{\vec{x}} = \dot{\hat{\vec{x}}} + \delta\dot{\vec{x}} = f(\hat{\vec{x}} + \delta\vec{x}, t) \quad (11)$$

Using Taylor series expansion

$$\begin{aligned} f(\hat{\vec{x}} + \delta\vec{x}, t) &= \dot{\hat{\vec{x}}} + \delta\dot{\vec{x}} = f(\hat{\vec{x}}, t) + \frac{\partial f(\vec{x}, t)}{\partial \vec{x}} \Big|_{\vec{x}=\hat{\vec{x}}} \delta\vec{x} + H.O.T \\ &\approx \dot{\hat{\vec{x}}} + \frac{\partial f(\vec{x}, t)}{\partial \vec{x}} \Big|_{\vec{x}=\hat{\vec{x}}} \delta\vec{x} \end{aligned}$$

Given a non-linear system  $\dot{\vec{x}} = f(\vec{x}, t)$

Let's assume we have an estimate of  $\vec{x}$ , i.e.,  $\hat{\vec{x}}$  such that  $\vec{x} = \hat{\vec{x}} + \delta\vec{x}$

$$\dot{\vec{x}} = \dot{\hat{\vec{x}}} + \delta\dot{\vec{x}} = f(\hat{\vec{x}} + \delta\vec{x}, t) \quad (11)$$

Using Taylor series expansion

$$\begin{aligned} f(\hat{\vec{x}} + \delta\vec{x}, t) &= \dot{\hat{\vec{x}}} + \delta\dot{\vec{x}} = f(\hat{\vec{x}}, t) + \frac{\partial f(\vec{x}, t)}{\partial \vec{x}} \Big|_{\vec{x}=\hat{\vec{x}}} \delta\vec{x} + H.O.T \\ &\approx \dot{\hat{\vec{x}}} + \frac{\partial f(\vec{x}, t)}{\partial \vec{x}} \Big|_{\vec{x}=\hat{\vec{x}}} \delta\vec{x} \end{aligned}$$

Given a non-linear system  $\dot{\vec{x}} = f(\vec{x}, t)$

Let's assume we have an estimate of  $\vec{x}$ , i.e.,  $\hat{\vec{x}}$  such that  $\vec{x} = \hat{\vec{x}} + \delta\vec{x}$

$$\dot{\vec{x}} = \dot{\hat{\vec{x}}} + \delta\dot{\vec{x}} = f(\hat{\vec{x}} + \delta\vec{x}, t) \quad (11)$$

Using Taylor series expansion

$$\begin{aligned} f(\hat{\vec{x}} + \delta\vec{x}, t) &= \dot{\hat{\vec{x}}} + \delta\dot{\vec{x}} = f(\hat{\vec{x}}, t) + \frac{\partial f(\vec{x}, t)}{\partial \vec{x}} \Big|_{\vec{x}=\hat{\vec{x}}} \delta\vec{x} + H.O.T \\ &\approx \dot{\hat{\vec{x}}} + \frac{\partial f(\vec{x}, t)}{\partial \vec{x}} \Big|_{\vec{x}=\hat{\vec{x}}} \delta\vec{x} \end{aligned}$$

$$\Rightarrow \delta\dot{\vec{x}} \approx \frac{\partial f(\vec{x}, t)}{\partial \vec{x}} \Big|_{\vec{x}=\hat{\vec{x}}} \delta\vec{x} \quad (12)$$

Initially the accelerometer and gyroscope measurements,  $\tilde{\vec{f}}_{ib}^b$  and  $\tilde{\vec{\omega}}_{ib}^b$ , respectively, will be modeled as

$$\tilde{\vec{f}}_{ib}^b = \vec{f}_{ib}^b + \Delta\vec{f}_{ib}^b \quad (13)$$

$$\tilde{\vec{\omega}}_{ib}^b = \vec{\omega}_{ib}^b + \Delta\vec{\omega}_{ib}^b \quad (14)$$

where  $\vec{f}_{ib}^b$  and  $\vec{\omega}_{ib}^b$  are the specific force and angular rates, respectively; and  $\Delta\vec{f}_{ib}^b$  and  $\Delta\vec{\omega}_{ib}^b$  represents the errors. In later lectures we will discuss more detailed description of these errors.

Initially the accelerometer and gyroscope measurements,  $\tilde{\vec{f}}_{ib}^b$  and  $\tilde{\vec{\omega}}_{ib}^b$ , respectively, will be modeled as

$$\tilde{\vec{f}}_{ib}^b = \vec{f}_{ib}^b + \Delta\vec{f}_{ib}^b \quad (13)$$

these terms may

$$\tilde{\vec{\omega}}_{ib}^b = \vec{\omega}_{ib}^b + \Delta\vec{\omega}_{ib}^b \quad (14)$$

be expanded further

where  $\vec{f}_{ib}^b$  and  $\vec{\omega}_{ib}^b$  are the specific force and angular rates, respectively; and  $\Delta\vec{f}_{ib}^b$  and  $\Delta\vec{\omega}_{ib}^b$  represents the errors. In later lectures we will discuss more detailed description of these errors.

## Accelerometers

$$\tilde{\vec{f}}_{ib}^b = \vec{b}_a + (\mathcal{I} + M_a) \vec{f}_{ib}^b + \vec{n}l_a + \vec{w}_a \quad (15)$$

## Gyroscopes

$$\tilde{\vec{\omega}}_{ib}^b = \vec{b}_g + (\mathcal{I} + M_g) \vec{\omega}_{ib}^b + G_g \vec{f}_{ib}^b + \vec{w}_g \quad (16)$$

## Accelerometers

$$\tilde{\vec{f}}_{ib}^b = \vec{b}_a + (\mathcal{I} + M_a) \vec{f}_{ib}^b + \vec{n}l_a + \vec{w}_a \quad (15)$$

Biases

## Gyroscopes

$$\tilde{\vec{\omega}}_{ib}^b = \vec{b}_g + (\mathcal{I} + M_g) \vec{\omega}_{ib}^b + G_g \vec{f}_{ib}^b + \vec{w}_g \quad (16)$$

## Accelerometers

$$\tilde{\vec{f}}_{ib}^b = \vec{b}_a + (\mathcal{I} + M_a) \vec{f}_{ib}^b + \vec{n}l_a + \vec{w}_a \quad (15)$$

Misalignment and SF Errors

## Gyroscopes

$$\tilde{\vec{\omega}}_{ib}^b = \vec{b}_g + (\mathcal{I} + M_g) \vec{\omega}_{ib}^b + G_g \vec{f}_{ib}^b + \vec{w}_g \quad (16)$$

## Accelerometers

$$\tilde{\vec{f}}_{ib}^b = \vec{b}_a + (\mathcal{I} + M_a) \vec{f}_{ib}^b + \vec{n} l_a + \vec{w}_a \quad (15)$$

Non-linearity

## Gyroscopes

$$\tilde{\vec{\omega}}_{ib}^b = \vec{b}_g + (\mathcal{I} + M_g) \vec{\omega}_{ib}^b + G_g \vec{f}_{ib}^b + \vec{w}_g \quad (16)$$

## Accelerometers

$$\tilde{\vec{f}}_{ib}^b = \vec{b}_a + (\mathcal{I} + M_a) \vec{f}_{ib}^b + \vec{n}l_a + \vec{w}_a \quad (15)$$

## Gyroscopes

G-Sensitivity

$$\tilde{\vec{\omega}}_{ib}^b = \vec{b}_g + (\mathcal{I} + M_g) \vec{\omega}_{ib}^b + G_g \vec{f}_{ib}^b + \vec{w}_g \quad (16)$$

## Accelerometers

$$\tilde{\vec{f}}_{ib}^b = \vec{b}_a + (\mathcal{I} + M_a) \vec{f}_{ib}^b + \vec{n} l_a + \vec{w}_a \quad (15)$$

Noise

## Gyroscopes

$$\tilde{\vec{\omega}}_{ib}^b = \vec{b}_g + (\mathcal{I} + M_g) \vec{\omega}_{ib}^b + G_g \vec{f}_{ib}^b + \vec{w}_g \quad (16)$$

- Position error

$$\delta \vec{r}_{\beta b}^{\gamma} = \vec{r}_{\beta b}^{\gamma} - \hat{\vec{r}}_{\beta b}^{\gamma} \quad (17)$$

- Velocity error

$$\delta \vec{v}_{\beta b}^{\gamma} = \vec{v}_{\beta b}^{\gamma} - \hat{\vec{v}}_{\beta b}^{\gamma} \quad (18)$$

- Specific force errors

$$\delta \vec{f}_{ib}^b = \vec{f}_{ib}^b - \hat{\vec{f}}_{ib}^b \quad (19)$$

$$\Delta_e \vec{f}_{ib}^b = \Delta \vec{f}_{ib}^b - \Delta \hat{\vec{f}}_{ib}^b = -\delta \vec{f}_{ib}^b \quad (20)$$

- Angular rate errors

$$\delta \vec{\omega}_{ib}^b = \vec{\omega}_{ib}^b - \hat{\vec{\omega}}_{ib}^b \quad (21)$$

$$\Delta_e \vec{\omega}_{ib}^b = \Delta \vec{\omega}_{ib}^b - \Delta \hat{\vec{\omega}}_{ib}^b = -\delta \vec{\omega}_{ib}^b \quad (22)$$

Define

$$\delta C_b^\gamma = C_b^\gamma \hat{C}_\gamma^b = e^{[\delta \vec{\psi}_{\gamma b}^\gamma \times]} \approx \mathcal{I} + [\delta \vec{\psi}_{\gamma b}^\gamma \times] \quad (23)$$

This is the error in attitude resulting from errors in estimating the angular rates.

The attitude error is a multiplicative small angle transformation from the actual frame to the computed frame

$$\hat{C}_b^\gamma = (\mathcal{I} - [\delta \vec{\psi}_{\gamma b}^\gamma \times]) C_b^\gamma \quad (24)$$

Similarly,

$$C_b^\gamma = (\mathcal{I} + [\delta \vec{\psi}_{\gamma b}^\gamma \times]) \hat{C}_b^\gamma \quad (25)$$

Similarly we can attempt to estimate the specific force and angular rate by applying correction based on our estimate of the error.

$$\hat{\tilde{f}}_{ib}^b = \tilde{f}_{ib}^b - \Delta \hat{f}_{ib}^b \quad (26)$$

$$\hat{\tilde{\omega}}_{ib}^b = \tilde{\omega}_{ib}^b - \Delta \hat{\omega}_{ib}^b \quad (27)$$

where  $\hat{\tilde{f}}_{ib}^b$  and  $\hat{\tilde{\omega}}_{ib}^b$  are the accelerometer and gyroscope estimated calibration values, respectively.