# Lecture <br> <br> Kalman Filtering Example 

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## EE 570: Location and Navigation

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## 1 Kalman Filter

## Remarks

- Kalman filter (KF) is optimal under the assumptions that the system is linear and the noise is uncorrelated
- Under these assumptions KF provides an unbiased and minimum variance estimate.
- If the Gaussian assumptions is not true, Kalman filter is biased and not minimum variance.
- If the noise is correlated we can augment the states of the system to maintain the the uncorrelated requirement of the system noise.


## 2 State Augmentation

## Correlated State Noise

Given a state space system

$$
\begin{gathered}
\dot{\vec{x}}_{1}(t)=F_{1}(t) \vec{x}_{1}(t)+G_{1}(t) \vec{w}_{1}(t) \\
\vec{y}_{1}(t)=H_{1}(t) \vec{x}_{1}(t)+\vec{v}(t)
\end{gathered}
$$

As we have seen the noise $\vec{w}_{1}(t)$ non-white, e.g., correlated Gaussian noise, and as such may be modeled as

$$
\begin{gathered}
\dot{\vec{x}}_{2}(t)=F_{2}(t) \vec{x}_{2}(t)+G_{2}(t) \vec{w}_{2}(t) \\
\vec{w}_{1}(t)=H_{2}(t) \vec{x}_{2}(t)
\end{gathered}
$$

## Correlated State Noise

Define a new augmented state

$$
\begin{equation*}
\vec{x}_{a u g}=\binom{\vec{x}_{1}(t)}{\vec{x}_{2}(t)} \tag{1}
\end{equation*}
$$

therefore,

$$
\dot{\vec{x}}_{a u g}=\binom{\dot{\vec{x}}_{1}(t)}{\overrightarrow{\vec{x}}_{2}(t)}=\left(\begin{array}{cc}
F_{1}(t) & G_{1} H_{2}(t)  \tag{2}\\
0 & F_{2}
\end{array}\right)\binom{\vec{x}_{1}(t)}{\vec{x}_{2}(t)}+\binom{0}{G_{2}(t)} \vec{w}_{2}(t)
$$

and

$$
\vec{y}(t)=\left(\begin{array}{ll}
H_{1} & 0 \tag{3}
\end{array}\right)\binom{\vec{x}_{1}(t)}{\vec{x}_{2}(t)}+\vec{v}(t)
$$

## Correlated Measurement Noise

Civen a state space system

$$
\begin{gathered}
\dot{\vec{x}}_{1}(t)=F_{1}(t) \vec{x}_{1}(t)+G_{1}(t) \vec{w}(t) \\
\vec{y}_{1}(t)=H_{1}(t) \vec{x}_{1}(t)+\vec{v}_{1}(t)
\end{gathered}
$$

In this case the measurement noise $\vec{v}_{1}$ may be correlated

$$
\begin{gathered}
\dot{\vec{x}}_{2}(t)=F_{2}(t) \vec{x}_{2}(t)+G_{2}(t) \vec{v}_{2}(t) \\
\vec{v}_{1}(t)=H_{2}(t) \vec{x}_{2}(t)
\end{gathered}
$$

## Correlated Measurement Noise

Define a new augmented state

$$
\begin{equation*}
\vec{x}_{a u g}=\binom{\vec{x}_{1}(t)}{\vec{x}_{2}(t)} \tag{4}
\end{equation*}
$$

therefore,

$$
\dot{\vec{x}}_{a u g}=\binom{\dot{\vec{x}}_{1}(t)}{\overrightarrow{\vec{x}}_{2}(t)}=\left(\begin{array}{cc}
F_{1}(t) & 0  \tag{5}\\
0 & F_{2}
\end{array}\right)\binom{\vec{x}_{1}(t)}{\vec{x}_{2}(t)}+\left(\begin{array}{cc}
G_{1}(t) & 0 \\
0 & G_{2}(t)
\end{array}\right)\binom{\vec{w}(t)}{\vec{v}_{2}}
$$

and

$$
\vec{y}(t)=\left(\begin{array}{ll}
H_{1} & H_{2} \tag{6}
\end{array}\right)\binom{\vec{x}_{1}(t)}{\vec{x}_{2}(t)}
$$

## 3 Example

Problem Statement
You are to design a system that estimates the position and velocity of a moving point in a straight line. You have:

1. an accelerometer corrupted with noise
2. an aiding sensor allowing you to measure absolute position that is also corrupted with noise. $\qquad$

## Specification

- Sampling Rate Fs $=100 \mathrm{~Hz}$.
- Accelerometer specs

1. $\mathrm{VRW}=1 \mathrm{mg} / \sqrt{H z}$.
2. $\mathrm{BI}=7 \mathrm{mg}$ with correlation time 6 s .

- Position measurement is corrupted with WGN. $\sim \mathcal{N}\left(0, \sigma_{p}^{2}\right)$, where $\sigma_{p}=2.5 \mathrm{~m}$
$\qquad$

True Acceleration and Acceleration with Noise


Aiding Position Measurement
Absolute position measurment corrupted with noise


## Different Approaches

1. Clean up the noisy input to the system.
2. Use Kalamn filtering techiques with

- A model of the system dyanmics (too ristrictive)
- A model of the error dyanmics and correct the system output in
- open-loop configuration, or
- closed-loop configuration.



## Closed-Loop Integration

If error estimates are fedback to correct the INS mechanization, a reset of the state estimates becomes necessary.


Kalman filter data flow


## Covariance Matrices

- State noise covariance matrix (continuous)

$$
\mathbb{E}\left\{\vec{w}(t) \hat{\vec{w}}^{T}(\tau)\right\}=Q(t) \delta(t-\tau)
$$

- State noise covariance matrix (discrete)

$$
\mathbb{E}\left\{\vec{w}_{k} \hat{\vec{w}}_{i}^{T}\right\}= \begin{cases}Q_{k} & i=k \\ 0 & i \neq k\end{cases}
$$

- Measurement noise covariance matrix

$$
\mathbb{E}\left\{\vec{v}_{k} \hat{\vec{v}}_{i}^{T}\right\}= \begin{cases}R_{k} & i=k \\ 0 & i \neq k\end{cases}
$$

- Error covariance matrix

$$
P_{k}=\mathbb{E}\left\{\left(\vec{x}_{k}-\hat{\vec{x}}_{k}\right)\left(\vec{x}_{k}-\hat{\vec{x}}_{k}\right)^{T}\right\}=\mathbb{E}\left\{\vec{e}_{k} \hat{\vec{e}}_{k}^{T}\right\}
$$

System modeling
The position, velocity and acceleration may be modeled using the following kinematic model.

$$
\begin{align*}
\dot{p}(t) & =v(t) \\
\dot{v}(t) & =a(t) \tag{7}
\end{align*}
$$

where $a(t)$ is the input.

## Measurement Model

Assuming that the accelerometer sensor measurement may be modeled as

$$
\begin{equation*}
\tilde{a}(t)=a(t)+b(t)+w_{a}(t) \tag{8}
\end{equation*}
$$

and the bias is Markov, therefore

$$
\begin{equation*}
\dot{b}(t)=-\frac{1}{T_{c}} b(t)+w_{b}(t) \tag{9}
\end{equation*}
$$

where both $w_{a}(t)$ and $w_{b}(t)$ are $W G N$. In addition we have the position measurment from which we can derive a delta position

$$
\begin{equation*}
\delta p(t)=p(t)-\hat{p}(t) \tag{10}
\end{equation*}
$$

where $\hat{p}$ is the derived position by double integrating the measured acceleration.

## Error Mechanization

Define the position and velocity error terms as

$$
\begin{align*}
\delta \dot{p}(t) & =\dot{p}(t)-\dot{\hat{p}}(t) \\
& =v(t)-\hat{v}(t)  \tag{11}\\
& =\delta v(t)
\end{align*}
$$

and

$$
\begin{align*}
\delta \dot{v}(t) & =\dot{v}(t)-\dot{\hat{v}}(t) \\
& =a(t)-\hat{a}(t)  \tag{12}\\
& =-b(t)-w_{a}(t)
\end{align*}
$$

where $b(t)$ is modeled as shown in Eq. 9

First Order Markov Noise
State Equation

$$
\begin{equation*}
\dot{b}(t)=-\frac{1}{T_{c}} b(t)+w_{b}(t) \tag{13}
\end{equation*}
$$

Autocorrelation Function

$$
\begin{equation*}
\mathbb{E}\{b(t) b(t+\tau)\}=\sigma^{2} e^{-|\tau| / T_{c}} \tag{14}
\end{equation*}
$$

where

$$
\begin{gather*}
\mathbb{E}\left\{w_{b}(t) w_{b}(t+\tau)\right\}=Q_{b}(t) \delta(t-\tau)  \tag{15}\\
Q_{b}(t)=\frac{2 \sigma_{B I}^{2}}{T_{c}} \tag{16}
\end{gather*}
$$

and $T_{c}$ is the correlation time and $\sigma_{B I}$ is the bias instability.
State Space Formulation

$$
\begin{align*}
\dot{\vec{x}}(t) & =\left(\begin{array}{c}
\delta \dot{p}(t) \\
\delta \dot{v}(t) \\
\dot{b}(t)
\end{array}\right)=\left(\begin{array}{ccc}
0 & 1 & 0 \\
0 & 0 & -1 \\
0 & 0 & -\frac{1}{T_{c}}
\end{array}\right)\left(\begin{array}{c}
\delta p(t) \\
\delta v(t) \\
b(t)
\end{array}\right)+\left(\begin{array}{ccc}
0 & 0 & 0 \\
0 & -1 & 0 \\
0 & 0 & 1
\end{array}\right)\left(\begin{array}{c}
0 \\
w_{a}(t) \\
w_{b}(t)
\end{array}\right)  \tag{17}\\
& =F(t) \vec{x}(t)+G(t) \vec{w}(t)
\end{align*}
$$

## Covariance Matrics

- The continuous state noise covariance matrix $Q(t)$ is

$$
Q(t)=\left(\begin{array}{ccc}
0 & 0 & 0  \tag{18}\\
0 & V R W^{2} & 0 \\
0 & 0 & \frac{2 \sigma_{B I}^{2}}{T c}
\end{array}\right)
$$

make sure that the $V R W$ and $\sigma_{B I}$ are converted to have SI units.

- The measurement noise covariance matrix is $R=\sigma_{p}^{2}$


## Discretization

Now we are ready to start the implementation but first we have to discretize the system.

$$
\begin{equation*}
\vec{x}(k+1)=\Phi(k) \vec{x}(k)+\vec{w}_{d} \tag{19}
\end{equation*}
$$

where

$$
\begin{equation*}
\Phi(k) \approx \mathcal{I}+F d t \tag{20}
\end{equation*}
$$

with the measurement equation

$$
\begin{equation*}
y(k)=H \vec{x}+w_{p}(k)=\delta p(k)+w_{p}(k) \tag{21}
\end{equation*}
$$

where $H=\left[\begin{array}{lll}1 & 0 & 0\end{array}\right]$. The discrete $Q_{d}$ is approximated as

$$
\begin{gather*}
Q_{k-1} \approx \frac{1}{2}\left[\Phi_{k-1} G\left(t_{k-1}\right) Q\left(t_{k-1}\right) G^{T}\left(t_{k-1}\right)\right) \Phi_{k-1}^{T}+  \tag{22}\\
\left.G\left(t_{k-1}\right) Q\left(t_{k-1}\right) G^{T}\left(t_{k-1}\right)\right] d t
\end{gather*}
$$

Discrete First Order Markov Noise

## State Equation

$$
\begin{equation*}
b_{k}=e^{-\frac{1}{T_{c}} d t} b_{k-1}+w_{b d, k-1} \tag{23}
\end{equation*}
$$

## System Covariance Matrix

$$
\begin{equation*}
Q_{b d}=\sigma_{B I}^{2}\left[1-e^{-\frac{2}{T_{c}} d t}\right] \tag{24}
\end{equation*}
$$

where $w_{b d}$ is the discrete noise for the bias.
You should use Eqs. 23 and 24 to overwrite their values in $\Phi$ and $Q_{d}$ since they don't need to be approximated.

Computed Position and Velocity
Using only the acceleration measurement and an integration approach to compute the velocity, then integrate again to get position.


Position


Velocity
$\qquad$

Approach 1 - Filtered input Filtered Accel Measurement


Approach 1 - Filtered input Position and Velocity


Position


Approach 1 - Filtered input Position and Velocity Errors


Position Error


Approach 2 - Open-Loop Compensation Position and Velocity
Open-loop Correction
Best estimate $=$ INS out $($ pos $\mathcal{E}$ vel $)+$ KF est error (pos $\mathcal{E}$ vel $)$


Position


Velocity

Approach 2 - Open-Loop Compensation Position and Velocity Errors


Approach 2 - Open-Loop Compensation Pos Error \& Bias Estimate



Bias

Approach 3 - Closed-Loop Compensation

## Closed-loop Correction

Best estimate $=$ INS out (pos,vel, $\mathcal{E}$ bias) + KF est error (pos, vel $\mathcal{E}$ bias) Use best estimate on next iteration of INS Accel estimate $=$ accel meas - est bias Reset state estimates before next call to KF


Position


Velocity


Approach 3 - Closed-Loop Compensation Pos Error \& Bias Estimate


Position Error


Bias

