

Lecture

Navigation Equations: ECI Mechanization

EE 570: Location and Navigation

Lecture Notes Update on February 20, 2014

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ECI Mechanization

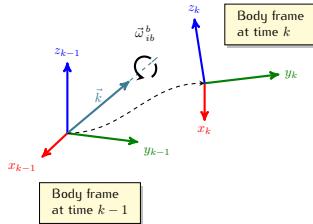
- Determine the position, velocity and attitude of the **body** frame *wrt* the **inertial** frame.
 - **Position** — Vector from the origin of the inertial frame to the origin of the body frame resolved in the inertial frame: \vec{r}_{ib}^i
 - **Velocity** — Velocity of the body frame *wrt* the inertial frame resolved in the inertial frame: \vec{v}_{ib}^i
 - **Attitude** — Orientation of the body frame *wrt* the inertial frame: C_b^i

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Attitude — Method A

- Body orientation frame at time "k" *wrt* time "k - 1"
 - $\Delta t = t_k - t_{k-1}$

$$\begin{aligned}\dot{C}_b^i &= C_b^i \Omega_{ib}^b \\ &= \lim_{\Delta \rightarrow 0} \left(\frac{C_b^i(k) - C_b^i(k-1)}{\Delta t} \right) = C_b^i(k-1) \Omega_{ib}^b \\ C_b^i(+)-C_b^i(-) &\approx C_b^i(-) \Omega_{ib}^b \Delta t \\ C_b^i(+) &\approx C_b^i(-) (\mathcal{I} + \Omega_{ib}^b \Delta t)\end{aligned}$$



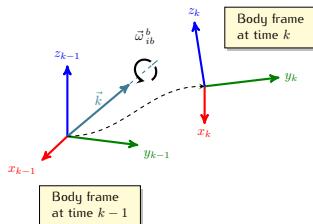
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Attitude — Method B

- Body orientation frame at time "k" *wrt* time "k - 1"
 - $\Delta t = t_k - t_{k-1}$

$$\begin{aligned}\vec{\omega}_{ib}^b \Delta t &= \vec{k} \Delta \theta \\ C_{b(k)}^i &= C_{b(k-1)}^i C_{b(k)}^{b(k-1)}\end{aligned}$$

$$\begin{aligned}C_{b(k)}^{b(k-1)} &= e^{\Omega_{ib}^b \Delta t} = e^{\kappa \Delta \theta} \\ &= \mathcal{I} + \kappa \Delta \theta + \frac{\kappa^2 \Delta \theta^2}{2!} + \frac{\kappa^3 \Delta \theta^3}{3!} + \dots \\ &= \mathcal{I} + \sin(\Delta \theta) \kappa + [1 - \cos(\Delta \theta)] \kappa^2 \\ C_b^i(+) &= C_b^i(-) C_{b(k)}^{b(k-1)} \\ &\approx C_b^i(-) (\mathcal{I} + \Omega_{ib}^b \Delta t)\end{aligned}$$



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Attitude — Method C

- Body orientation frame at time "k" wrt time "k - 1"

$$-\Delta t = t_k - t_{k-1}$$

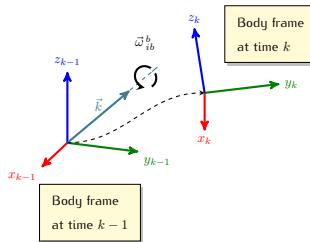
$$\vec{\omega}_{ib}^b \Delta t = \vec{k} \Delta \theta$$

$$\bar{q}_{b(k)}^i = \bar{q}_{b(k-1)}^i \otimes \bar{q}_{b(k)}^{b(k-1)}$$

$$\bar{q}_{b(k)}^{b(k-1)} = \begin{bmatrix} \cos(\frac{\Delta\theta}{2}) \\ \vec{k} \sin(\frac{\Delta\theta}{2}) \end{bmatrix}$$

$$\bar{q}_b^i(+) = \bar{q}_b^i(-) \otimes \bar{q}_{b(k)}^{b(k-1)}$$

Need to periodically renormalize \bar{q}



Attitude Update— Summary

- High fidelity

$$C_b^i(+) = C_b^i(-) [\mathcal{I} + \sin(\Delta\theta)\mathfrak{K} + [1 - \cos(\Delta\theta)]\mathfrak{K}^2] \quad (1)$$

or

$$\bar{q}_b^i(+) = \bar{q}_b^i(-) \otimes \begin{bmatrix} \cos(\frac{\Delta\theta}{2}) \\ \vec{k} \sin(\frac{\Delta\theta}{2}) \end{bmatrix} \quad (2)$$

- Low fidelity

$$C_b^i(+) \approx C_b^i(-) (\mathcal{I} + \Omega_{ib}^b \Delta t) \quad (3)$$

Steps 2–4

2. Specific force transformation

- Simply coordinatize the specific force

$$\vec{f}_{ib}^i = C_b^i(+) \vec{f}_{ib}^b \quad (4)$$

3. Velocity update

- Assuming that we are in space (i.e., no centrifugal component)

$$\vec{a}_{ib}^i = \vec{f}_{ib}^i + \vec{\gamma}_{ib}^i \quad (5)$$

- Thus, by simple numerical integration

$$\vec{v}_{ib}^i(+) = \vec{v}_{ib}^i(-) + \vec{a}_{ib}^i \Delta t \quad (6)$$

4. Position update

- by simple numerical integration

$$\vec{r}_{ib}^i(+) = \vec{r}_{ib}^i(-) + \vec{v}_{ib}^i(-) \Delta t + \vec{a}_{ib}^i \frac{\Delta t^2}{2} \quad (7)$$

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ECI Mechanization Summary

$$C_b^i(+) = C_b^i(-) [\mathcal{I} + \sin(\Delta\theta)\vec{\kappa} + [1 - \cos(\Delta\theta)] \vec{\kappa}^2]$$

or

$$C_b^i(+) \approx C_b^i(-) (\mathcal{I} + \Omega_{ib}^b \Delta t)$$

or

$$\bar{q}_b^i(+) = \bar{q}_b^i(-) \otimes \begin{bmatrix} \cos(\frac{\Delta\theta}{2}) \\ \vec{k} \sin(\frac{\Delta\theta}{2}) \end{bmatrix}$$

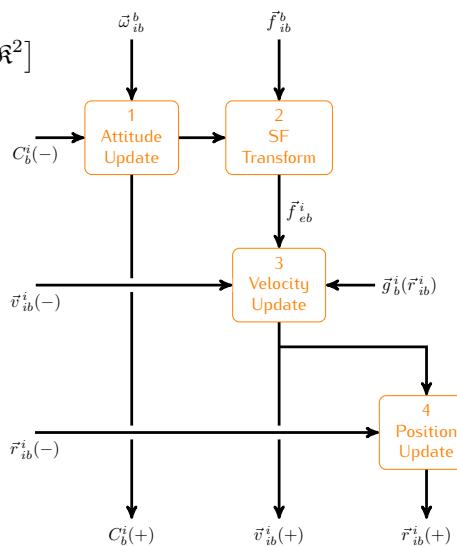
and

$$\vec{f}_{ib}^i = C_b^i(+) \vec{f}_{ib}^b$$

$$\vec{a}_{ib}^i = \vec{f}_{ib}^i + \vec{\gamma}_{ib}^i$$

$$\vec{v}_{ib}^i(+) = \vec{v}_{ib}^i(-) + \vec{a}_{ib}^i \Delta t$$

$$\vec{r}_{ib}^i(+) = \vec{r}_{ib}^i(-) + \vec{v}_{ib}^i(-) \Delta t + \vec{a}_{ib}^i \frac{\Delta t^2}{2}$$



ECI Mechanization — Continuous Case

- In continuous time notation

- Attitude: $\dot{C}_b^i = C_b^i \Omega_{ib}^b$ or $\dot{q}_b^i = \frac{1}{2}[\vec{\omega}_{ib}^b \otimes] \bar{q}_b^i(t)$
- Velocity: $\dot{\vec{v}}_{ib}^i = C_b^i \vec{f}_{ib}^b + \vec{\gamma}_{ib}^i$
- Position: $\dot{\vec{r}}_{ib}^i = \vec{v}_{ib}^i$

- In State-space notation

$$\begin{bmatrix} \dot{\vec{r}}_{ib}^i \\ \dot{\vec{v}}_{ib}^i \\ \dot{C}_b^i \end{bmatrix} = \begin{bmatrix} \vec{v}_{ib}^i \\ C_b^i \vec{f}_{ib}^b + \vec{\gamma}_{ib}^i \\ C_b^i \Omega_{ib}^b \end{bmatrix} \quad (8)$$

or

$$\begin{bmatrix} \dot{\vec{r}}_{ib}^i \\ \dot{\vec{v}}_{ib}^i \\ \dot{q}_b^i \end{bmatrix} = \begin{bmatrix} \vec{v}_{ib}^i \\ C_b^i \vec{f}_{ib}^b + \vec{\gamma}_{ib}^i \\ \frac{1}{2}[\vec{\omega}_{ib}^b \otimes] \bar{q}_b^i(t) \end{bmatrix} \quad (9)$$

Appendix

$$[\bar{q} \otimes] = \begin{bmatrix} q_s & -q_x & -q_y & -q_z \\ q_x & q_s & -q_z & q_y \\ q_y & q_z & q_s & -q_x \\ q_z & -q_y & q_x & q_s \end{bmatrix}$$

$$[\bar{q} \circledast] = \begin{bmatrix} q_s & -q_x & -q_y & -q_z \\ q_x & q_s & q_z & -q_y \\ q_y & -q_z & q_s & q_x \\ q_z & q_y & -q_x & q_s \end{bmatrix}$$

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